APPENDIX J

ENVIRONMENTAL NOISE ASSESSMENT

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BASCOM AVENUE MEDICAL OFFICE BUILDING 200 NORTH BASCOM AVENUE SAN JOSE, CALIFORNIA

WJVA Report No. 21-08

PREPARED FOR

EMC PLANNING 301 LIGHTHOUSE AVENUE, SUITE C MONTEREY, CA 93940

PREPARED BY

WJV ACOUSTICS, INC. VISALIA, CALIFORNIA



MARCH 16, 2021

1. <u>INTRODUCTION</u>

Project Description

The proposed project would consist of the construction of a four story, 34,987 square-foot medical office building located at 200 North Bascom Avenue, in San Jose, California. The project would include two levels of below grade parking as well as surface parking at the rear of the building. The project site plan is provided as Figure 1.

Environmental Noise Assessment

This environmental noise assessment has been prepared to determine if significant noise impacts would be produced by the project and to describe mitigation measures for noise if significant impacts are determined. The environmental noise assessment, prepared by WJV Acoustics, Inc. (WJVA), is based upon the project site plan design and construction package prepared by Ratcliff Architecture (dated 1-2-21) project-related traffic data provided by TJKM Transportation Consultants, Inc. and a project site visit on February 10 and 11, 2021. Revisions to the site plan, project-related traffic data or other project-related information available to WJVA at the time the analysis was prepared may require a reevaluation of the findings and/or recommendations of the report.

Appendix A provides definitions of the acoustical terminology used in this report. Unless otherwise stated, all sound levels reported in this analysis are A-weighted sound pressure levels in decibels (dB). A-weighting de-emphasizes the very low and very high frequencies of sound in a manner similar to the human ear. Most community noise standards utilize A-weighted sound levels, as they correlate well with public reaction to noise. Appendix B provides typical A-weighted sound levels for common noise sources.

In terms of human perception, a 5 dB increase or decrease is considered to be a noticeable change in noise levels. Additionally, a 10 dB increase or decrease is perceived by the human ear as half as loud or twice as loud. In terms of perception, generally speaking the human ear cannot perceive an increase (or decrease) in noise levels less than 3 dB.

2. THRESHOLDS OF SIGNIFICANCE

The CEQA Guidelines apply the following questions for the assessment of significant noise impacts for a project:

- a. Would the project result in generation of a substantial temporary or permanent increase in ambient noise levels in the vicinity of the project in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies?
- b. Would the project result in generation of excessive groundborne vibration or groundborne noise levels?
- c. For a project located within the vicinity of a private airstrip or an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, would the project expose people residing or working in the project area to excessive noise levels?

a. Noise Level Standards

City of San Jose

General Plan

The Environmental Leadership Chapter of the Envision San Jose 2040 General Plan¹ (adopted November 1, 2011) establishes land use compatibility criteria in terms of the Day-Night Average Level (L_{dn}/DNL). The L_{dn} represents the time-weighted energy average noise level for a 24-hour day, with a 10 dB penalty added to noise levels occurring during the nighttime hours (10:00 p.m.-7:00 a.m.). The L_{dn} represents cumulative exposure to noise over an extended period of time and are therefore calculated based upon *annual average* conditions. The General Plan establishes noise exposure criteria for specific land use types. The Noise level criteria established in the General Plan are provided below.

Goal EC-1 – Community Noise Levels and Land Use Compatibility

Minimize the impact of noise on people through noise reduction and suppression techniques, and through appropriate land use policies.

Policies – Community Noise Levels and Land Use Compatibility

EC-1.1 Locate new development in areas where noise levels are appropriate for the proposed uses. Consider federal, state and City noise standards and guidelines as a part of new development review. Applicable standards and guidelines for land uses in San José include:

Interior Noise Levels

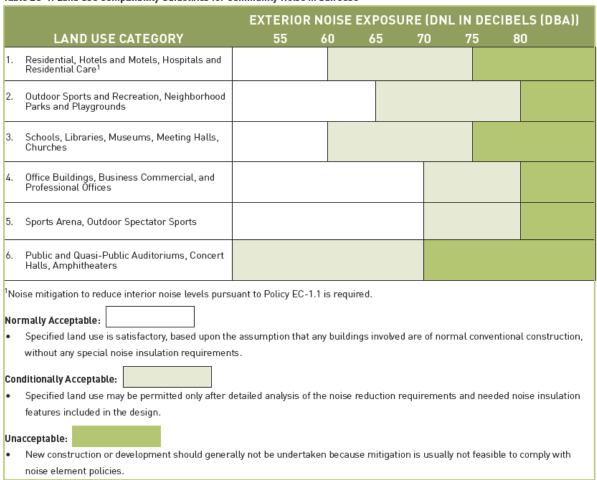
• The City's standard for interior noise levels in residences, hotels, motels, residential care facilities, and hospitals is 45 dBA DNL. Include appropriate site and building design, building construction and noise attenuation techniques in new development to meet this standard. For sites with exterior noise levels of 60 dBA DNL or more, an acoustical analysis following protocols in the City-adopted California Building Code is required to demonstrate that development projects can meet this standard. The acoustical analysis shall base required noise attenuation techniques on expected Envision General Plan traffic volumes to ensure land use compatibility and General Plan consistency over the life of this plan.

Exterior Noise Levels

- The City's acceptable exterior noise level objective is 60 dBA DNL or less for residential and most institutional land uses (Table EC-1). The acceptable exterior noise level objective is established for the City, except in the environs of the San José International Airport and the Downtown, as described below:
- For new multi-family residential projects and for the residential component of mixed-use development, use a standard of 60 dBA DNL in usable outdoor activity areas, excluding balconies and residential stoops and porches facing existing roadways. Some common use areas that meet the 60 dBA DNL exterior standard will be available to all residents. Use noise attenuation techniques such as shielding by buildings and structures for outdoor common use areas. On sites subject to aircraft overflights or adjacent to elevated roadways, use noise attenuation techniques to achieve the 60 dBA DNL standard for noise from sources other than aircraft and elevated roadway segments.
- For single family residential uses, use a standard of 60 dBA DNL for exterior noise in private usable outdoor activity areas, such as backyards.
- For

Although not explicitly stated in the General Plan, exterior noise level standards are typically applied to "outdoor activity areas". Outdoor activity areas are generally considered to be backyards of single-family residential land uses, common use outdoor areas and individual patios and balconies of multi-family residential land uses, and common use outdoor areas for transient lodging land uses.

Table EC-1: Land Use Compatibility Guidelines for Community Noise in San José



EC-1.2 Minimize the noise impacts of new development on land uses sensitive to increased noise levels (Categories 1, 2, 3 and 6) by limiting noise generation and by requiring use of noise attenuation measures such as acoustical enclosures and sound barriers, where feasible. The City considers significant noise impacts to occur if a project would:

- Cause the DNL at noise sensitive receptors to increase by five dBA DNL or more where the noise levels would remain "Normally Acceptable"
- Cause the DNL at noise sensitive receptors to increase by three dBA DNL or more where the noise levels would equal or exceed the "Normally Acceptable" level.

EC-1.3 Mitigate noise generation of new nonresidential land uses to 55 dBA DNL at the property line when located adjacent to existing or planned noise sensitive residential and public/quasipublic land uses.

Municipal Code

Section 20.40.600 (Performance Standards) of the City of San Jose Municipal Code provides additional noise standards for stationary noise sources applicable to the project. The Municipal Code states that noise levels associated with commercially zoned properties cannot exceed 55 dB L_{max} (maximum) at adjacent residential property lines.

b. Construction Noise and Vibration

The General Plan provides establishes the following guidelines related to construction activities:

EC-1.7 Require construction operations within San José to use best available noise suppression devices and techniques and limit construction hours near residential uses per the City's Municipal Code. The City considers significant construction noise impacts to occur if a project located within 500 feet of residential uses or 200 feet of commercial or office uses would:

• Involve substantial noise generating activities (such as building demolition, grading, excavation, pile driving, use of impact equipment, or building framing) continuing for more than 12 months.

For such large or complex projects, a construction noise logistics plan that specifies hours of construction, noise and vibration minimization measures, posting or notification of construction schedules, and designation of a noise disturbance coordinator who would respond to neighborhood complaints will be required to be in place prior to the start of construction and implemented during construction to reduce noise impacts on neighboring residents and other uses.

Additionally, section 20.100.450 of the City of San Jose Municipal code provides the following:

 Unless otherwise expressly allowed in a development permit or other planning approval, no applicant or agent of an applicant shall suffer or allow any construction activity on a site located within 500 feet of a residential unit before 7:00 a.m. or after 7:00 p.m., Monday through Friday, or at any time on weekends.

The General Plan also provides some guidance and guidelines associated with vibration.

Goal EC-2 - Vibration

Minimize vibration impacts on people, residences, and business operations.

EC-2.3

Require new development to minimize continuous vibration impacts to adjacent uses during demolition and construction. For sensitive historic structures, including ruins and ancient monuments or building that are documented to be structurally weakened, a continuous vibration limit of 0.08 in/sec PPV (peak particle velocity) will be used to minimize the potential for cosmetic damage to a building. A continuous vibration limit of 0.20 in/sec PPV will be used to minimize the potential for cosmetic damage at buildings of normal conventional construction. Equipment or activities typical of generating continuous vibration include but are not limited to: excavation equipment; static compaction equipment; vibratory pile drivers; pile-extraction equipment; and vibratory compaction equipment. Avoid use of impact pile drivers within 125 feet of any buildings, and within 300 feet of historical buildings, or buildings in poor condition. On a project-specific basis, this distance of 300 feet may be reduced where warranted by a technical study by a qualified professional that verifies that there will be virtually no risk of cosmetic damage to sensitive buildings from the new development during demolition and construction. Transient vibration

impacts may exceed a vibration limit of 0.08 in/sec PPV only when and where warranted by a technical study by a qualified professional that verifies that there will be virtually no risk of cosmetic damage to sensitive buildings from the new development during demolition and construction.

Additional guidance is provided by the Caltrans Transportation and Construction Vibration Guidance Manual³. The Manual provides guidance for determining annoyance potential criteria and damage potential threshold criteria. These criteria are provided below in Table I and Table II, and are presented in terms of peak particle velocity (PPV) in inches per second (in/sec).

	TABLE I			
GUIDELINE \	IBRATION ANNOYANCE POTENT			
	Maximum PPV (in/sec)			
Human Response	Transient Sources	Continuous/Frequent Intermittent Sources		
Barely Perceptible	0.04	0.01		
Distinctly Perceptible	0.25	0.04		
Strongly Perceptible	0.9	0.1		
Severe	2.0	0.4		
Source: Caltrans				

TABLE GUIDELINE VIBRATION DAMAGE PO		CRITERIA
	Maximum	PPV (in/sec)
Structure and Condition	Transient Sources	Continuous/Frequent Intermittent Sources
Extremely fragile, historic buildings, ancient monuments	0.12	0.08
Fragile buildings	0.2	0.1
Historic and some old buildings	0.5	0.25
Older residential structures	0.5	0.3
New residential structures	1.0	0.5
Modern industrial/commercial buildings	2.0	0.5
Source: Caltrans		

3. SETTING

The project site is located at 200 N. Bascom Avenue, north of Forest Avenue, in San Jose, California. Existing single-family residences border the project site to the north, although some of the residences are currently being utilized as office uses. There are additional single-family residential land uses to the south and east of the project site with commercial and office uses to the north and west of the project site.

a. Background Noise Level Measurements

Existing ambient noise levels in the project vicinity are dominated by vehicle traffic noise sources. Other sources of noise observed during the site visit include aircraft overflights associated with Norman Y Mineta San Jose International Airport, landscaping activities, construction activities, human voices, barking dogs, birds and other sources of noise typical of urban environments.

Measurements of existing ambient noise levels in the project vicinity were conducted on February 10 and 11, 2021. Long-term (24-hour) ambient noise level measurements were conducted at one (1) location (sites LT-1). Site LT-1 was located at the rear of the existing structure, within the project site, in the vicinity of the adjacent single-family residential land use to the east. Site LT-1 was exposed to traffic noise associated with vehicles on nearby local roadways, aircraft overflights and noise associated with residential activities, including construction and landscaping activities.

Additionally, short-term (15-minute) ambient noise level measurements were conducted at five (5) locations (Sites ST-1 through ST-5). Two (2) individual measurements were taken at each of the five short-term sites to quantify ambient noise levels in the morning and afternoon hours. The project vicinity and locations of the noise monitoring sites are shown on Figure 2.

Noise monitoring equipment consisted of Larson-Davis Laboratories Model LDL-820 sound level analyzers equipped with B&K Type 4176 1/2" microphones. The equipment complies with the specifications of the American National Standards Institute (ANSI) for Type I (Precision) sound level meters. The meters were calibrated with a B&K Type 4230 acoustic calibrator to ensure the accuracy of the measurements.

Measured hourly energy average noise levels (L_{eq}) at site LT-1 ranged from a low of 42.6 dB between midnight and 1:00 a.m. to a high of 57.4 dB between noon and 1:00 p.m. Hourly maximum (L_{max}) noise levels at site LT-1 ranged from 57.1 to 80.4 dB. Residual noise levels at the monitoring site, as defined by the L_{90} statistical descriptor ranged from 39.2 to 52.2 dB. The L_{90} is a statistical descriptor that defines the noise level exceeded 90% of the time during each hour of the sample period. The L_{90} is generally considered to represent the residual (or background) noise level in the absence of identifiable single noise events from traffic, aircraft and other local noise sources. The measured L_{dn} value at site LT-1 during the 24-hour noise measurement period was 56.4 dB L_{dn} . Figure 3 graphically depicts hourly variations in ambient noise levels at the LT-1 long-term monitoring site as well as a site photograph.

The short-term site noise measurement data included energy average (L_{eq}) maximum (L_{max}) as well as five (5) individual statistical parameters. Observations were made of the dominant noise sources affecting the measurements. The statistical parameters describe the percent of time a noise level was exceeded during the measurement period. Table III summarizes short-term noise measurement results.

TABLE III

SUMMARY OF SHORT-TERM NOISE MEASUREMENT DATA 200 N. BASCOM AVENUE MEDICAL OFFICE BUILDING SAN JOSE, CALIFORNIA FEBRUARY 10 & 11, 2020

C'A-		A-Weighted Decibels, dBA						Sources	
Site	Time	L _{eq}	L _{max}	L ₂	L ₈	L ₂₅	L ₅₀	L ₉₀	Sources
ST-1	8:05 a.m.	66.2	74.2	72.0	69.8	66.8	64.6	62.2	TR, AC
ST-1	4:55 p.m.	67.0	74.1	72.4	71.1	65.6	63.8	58.7	TR, AC,
ST-2	8:20 a.m.	54.9	65.6	62.2	60.8	55.0	52.1	47.5	TR, B, C
ST-2	5:20 p.m.	56.4	72.4	63.0	62.4	56.6	53.7	48.2	TR, AC
ST-3	8:45 a.m.	51.8	63.2	61.1	54.1	51.5	49.0	46.3	TR, C, L
ST-3	5:45 p.m.	53.2	66.6	61.4	56.2	52.0	48.7	45.5	TR, B, V
ST-4	9:05 a.m.	55.0	66.2	63.5	60.3	54.0	51.1	48.3	TR, B, AC
ST-4	6:05 p.m.	54.1	62.4	62.1	58.7	53.0	50.0	46.2	TR, V
ST-5	9:25 a.m.	67.1	77.0	75.3	71.3	67.6	63.2	56.7	TR, L
ST-5	6:25 p.m.	67.0	74.9	72.4	71.1	65.1	62.8	56.1	TR, AC, V

TR: Traffic AC: Aircraft V: Voices B: Birds R: L: Landscaping Activities C: Construction

Source: WJV Acoustics, Inc.

Short-term noise measurements were conducted for 15-minute periods. Sites ST-1 and ST-5 were located adjacent to N. Bascom Avenue, where traffic noise was elevated, while sites ST-2, ST-3 and ST-4 and ST-5 were located in the vicinity of predominantly residential uses. All of the five short-term monitoring sites were exposed to noise from traffic sources, construction noise sources, aircraft overflights and other sources typical of an urban residential environment (barking dogs, birds, landscaping activities, etc.).

4. PROJECT IMPACTS AND MITIGATION MEASURES

a. Project Traffic Noise Impacts on Existing Noise-Sensitive Land Uses Outside Project Site (No Impact)

WJVA utilized the FHWA Traffic Noise Model⁴ to quantify expected project-related increases in traffic noise exposure at representative noise-sensitive receptor locations in the project vicinity. Traffic noise exposure levels for Existing, Existing Plus Project, Cumulative No Project and Cumulative Plus Project traffic conditions were calculated based upon the FHWA Model and traffic volumes provided by TJKM Transportation Consultants. Cumulative traffic volumes reflect projected traffic volumes on the planned roadway network with completion of the pending developments in the area as well as the proposed project and approved developments. The day/night distribution of traffic and the percentages of trucks on the roadways used for modeling were obtained from previous studies WJVA has conducted along similar roadways. The Noise modeling assumptions used to calculate project traffic noise are provided as Appendix C.

Project-related significant impacts would occur if an increase in traffic noise associated with the project would result in noise levels exceeding the City's applicable noise level standards at the location(s) of sensitive receptors. The City of San Jose also considers a significant impact to occur if the project were to cause the DNL at noise sensitive receptors to increase by five (5) dBA DNL or more where the noise levels would remain "Normally Acceptable" or cause the DNL at noise sensitive receptors to increase by three (3) dBA DNL or more where the noise levels would equal or exceed the "Normally Acceptable" level.

This analysis of project traffic noise focuses on potential impacts to residential land uses, as they represent the most restrictive noise level criteria by land use type provided in the General Plan. The City's exterior noise level standard for residential land uses is $60 \, \text{dB} \, \text{L}_{dn}$. Traffic noise was modeled at ten (10) receptor locations (R-1 through R-10). The ten modeled receptors are located at roadway setback distances representative of the sensitive receptors (residences) along each analyzed roadway segment. The receptor locations are described below and provided graphically on Figure 4.

- R-1: Approximately 170 feet from the centerline of Naglee Ave., east of Dana Ave.
- R-2: Approximately 80 feet from the centerline of Dana Ave., north of Naglee Ave.
- R-3: Approximately 140 feet from the centerline of Naglee Ave., east of Bascom Ave.
- R-4: Approximately 75 feet from the centerline of Bascom Ave., north of Naglee Ave.
- R-5: Approximately 130 feet from the centerline of Bascom Ave., south of Naglee Ave.
- R-6: Approximately 60 feet from the centerline of Bascom Ave., north of Hedding St.
- R-7: Approximately 140 feet from the centerline of Hedding St., east of Bascom Ave.
- R-8: Approximately 120 feet from the centerline of Hedding St., west of Bascom Ave.
- R-9: Approximately 160 feet from the centerline of Stevens Creek Blvd., west of Bascom Ave.
- R-10: Approximately 130 feet from the centerline of Bascom Ave., south of San Carlos Ave.

Table IV provides a comparison of traffic noise levels at the ten modeled receptor locations for Existing, Existing Plus Project, Cumulative and Cumulative Plus Project traffic conditions. Noise

levels described in Table IV do not take into account any localized acoustic shielding that may result from intervening topography, existing buildings or existing sound walls, and should be considered a worst-case assessment of traffic noise exposure levels. As described in Table IV, project-related traffic is not expected to result in noise levels at any sensitive receptors to exceed the City's noise level standard, nor result in an increase of 3 dB in any sensitive receptor locations where noise levels already exceed the County's noise level standard without the implementation of the project. Project-related traffic is not expected to increase traffic noise levels at any roadway. Therefore, project-related increases in traffic noise exposure are considered to be no impact.

TABLE IV

PROJECT-RELATED INCREASES IN TRAFFIC NOISE, dB, Ldn
200 N. BASCOM AVENUE MEDICAL OFFICE BUILDING

Modeled Receptor	Existing	Existing Plus Project	Cumulative	Cumulative Plus Project	Change (Maximum)	Significant Impact?
R-1	57	57	57	57	0	No
R-2	54	54	55	55	0	No
R-3	59	59	59	59	0	No
R-4	64	64	64	64	0	No
R-5	61	61	61	61	0	No
R-6	66	66	66	66	0	No
R-7	58	58	58	58	0	No
R-8	59	59	59	59	0	No
R-9	58	58	59	59	0	No
R-10	62	62	62	62	0	No

Source: WJV Acoustics, Inc.

Hexagon Transportation Consultants

b. Noise Impacts from On-Site Noise Sources (No Impact)

Sources of operational noise from the proposed project would typically be limited to parking lot vehicle movements, outdoor human activity and Mechanical/HVAC systems. The project design does not include any loading docks or trash compactors, and truck deliveries would not be expected to occur at the site.

The project would incorporate approximately 60 parking spaces, 58 of which will be located at two underground levels and two (2) van accessible parking spaces will be located at the rear of the building at first floor level. Additionally, four (4) motorcycle parking spaces will be located at first floor level at the rear of the building. Access to the below grade parking levels is from Bascom Avenue.

Noise due to traffic in parking lots is typically limited by low speeds and is not usually considered to be significant. Human activity in parking lots that can produce noise includes voices, stereo systems

and the opening and closing of car doors and trunk lids. The noise levels associated with these activities cannot be precisely defined due to variables such as the number of parking movements, time of day and other factors. It is typical for a passing car in a parking lot to produce a maximum noise level of 60 to 65 dBA at a distance of 50 feet, which is comparable to the level of a raised voice. However, the majority project parking spaces will be located below grade, within the structure of the building, and noise associated with vehicle movements would not be audible at any nearby sensitive receptor locations. Noise levels associated with first floor level parking at the rear of the building would not exceed existing (without project) ambient noise levels at the adjacent residential land uses.

The project would include roof-mounted Mechanical/HVAC units on the building, with a mechanical screen parapet around the area. Based upon data collected by WJVA for previous acoustical studies, it is estimated that noise levels from roof-mounted HVAC units at the closest off-site sensitive receptor locations to the project site (nearby residential land uses) would be in the range of 45-50 dBA. These levels would generally not be audible above existing ambient noise levels at adjacent land-uses and would not exceed any City of San Jose noise level standards.

The project would also include two (2) outdoor rooftop terrace areas. Noise associated with rooftop terrace use would generally be limited to that of human voice, typically approximately 60 dB at a distance of six (6) feet from the source. The terrace areas would be located at least 75 feet from the closest residential land use, at which distance noise levels from a human voice would be approximately 38 dB, below City of San Jose noise standards and below existing (without project) ambient noise levels.

c. Noise From Construction (Less Than Significant With Mitigation)

Policy EC-1.7 of the General Plan requires construction operations within the City to use best available noise suppression devices and techniques and limit construction hours near residential uses per the City's Municipal Code. The City considers significant construction noise impacts to occur if a project located within 500 feet of residential uses or 200 feet of commercial or office uses would involve substantial noise generating activities (such as building demolition, grading, excavation, pile driving, use of impact equipment, or building framing) continuing for more than twelve months.

For such large or complex projects, a construction noise logistics plan that specifies hours of construction, noise and vibration minimization measures, posting or notification of construction schedules, and designation of a noise disturbance coordinator who would respond to neighborhood complaints will be required to be in place prior to the start of construction and implemented during construction to reduce noise impacts on neighboring residents and other uses.

Section 20.100.450 of the City of San Jose Municipal code requires any construction activity on a site located within 500 feet of a residential unit must occur between the hours of 7:00 a.m. to 7:00 p.m., Monday through Friday, and no construction activities are allowed on weekends.

Construction noise would occur at various locations within the project site through the build-out period. The distance from the closest residences to the project site is approximately 25 feet. Table V provides typical construction-related noise levels at distances of 25feet, 50 feet, and 100 feet.

	TABL TYPICAL CONSTRUC MAXIMUM NOISE	CTION EQUIPMENT E LEVELS, dBA	
Type of Equipment	25 Ft.	50 Ft.	100 Ft.
Concrete Saw	96	90	84
Crane	87	81	75
Excavator	87	81	75
Front End Loader	85	79	73
Jackhammer	95	89	83
Paver	83	77	71
Pneumatic Tools	91	85	79
Dozer	87	81	76
Rollers	86	80	74
Trucks	92	86	80
Pumps	86	80	74
Scrapers	93	87	81
Portable Generators	87	81	74
Backhoe	92	86	80
Grader	92	86	80

Source: FHWA

Noise Control for Buildings and Manufacturing Plants, Bolt, Beranek & Newman, 1987

Noise impacts associated with construction activities typically depend on the noise levels generated by the type of equipment in use, the duration of usage of the equipment and the distance at which the equipment is used in respect to nearby sensitive receptors. Noise impacts typically occur when construction activities occur beyond the limited allowable hours of construction. Construction activities will occur within 500 feet of residential land uses and within 200 feet of office uses. However, the anticipated duration of project construction (including demolition) is anticipated to be less than twelve months.

Construction noise is typically not considered to be a significant impact if construction is limited to the daytime hours and construction equipment is adequately maintained and muffled. Extraordinary noise-producing activities (e.g., pile driving) are not anticipated. In this case, all project construction activity must be confined to the hours of 7:00 a.m. to 7:00 p.m., Monday through Friday. Construction noise impacts could result in annoyance or sleep disruption for nearby residents if nighttime operations were to occur or if equipment is not properly muffled or maintained. If construction activities that involved substantial noise generating activities (such as

building demolition, grading, excavation, pile driving, use of impact equipment, or building framing) for a duration greater than twelve months, a substantial impact would occur.

Potential Impact: If the overall duration of construction activities were to occur over a period greater than twelve months, a noise impact would occur, as determined by the City of San Jose Municipal Code.

Mitigation Measure: The anticipated duration of project construction (including demolition) is less than twelve months. However, If project construction were to occur for a duration greater than twelve months, the project team must provide a construction noise logistics plan that specifies hours of construction, noise and vibration minimization measures, posting or notification of construction schedules, and designation of a noise disturbance coordinator who would respond to neighborhood complaints will be required to be in place prior to the start of construction and implemented during construction to reduce noise impacts on neighboring residents and other uses.

Vibration Impacts (Less Than Significant With Mitigation)

The dominant sources of man-made vibration are sonic booms, blasting, pile driving, pavement breaking, demolition, diesel locomotives, and rail-car coupling. The highest levels of construction-related vibration are typically associated with pile driving and the use of vibratory rollers. While the project could include pavement breaking and demolition activities (jackhammer), project demolition and construction would not require pile driving.

The project would use a vibratory roller, however, vibration levels associated with a vibratory roller would not exceed City of San Jose vibration standard of 20 PPV (in/sec) as long as a distance of thirty (30) feet is maintained between the activity and existing structures (at 30 feet the associated vibratory roller vibration level would be approximately 0.172 PPV). Regarding pile driving activities, the City of San Jose General Plan states "Avoid use of impact pile drivers within 125 feet of any buildings, and within 300 feet of historical buildings, or buildings in poor condition". According to the project applicant, pile driving activities would not occur during the construction of the project.

Vibration from demolition and construction activities could be detected at the closest sensitive land uses, especially during demolition (pavement/concrete breaking), movements by heavy equipment or loaded trucks and during some paving activities (if they were to occur). Typical vibration levels at distances of 25 feet, 100 feet and 300 feet are summarized by Table VI. These levels would not be expected to exceed any significant threshold levels for annoyance or damage, as provided above in Table I and Table II (vibratory roller activities must not occur within 30 feet of existing structures).

TABLE VI
TYPICAL VIBRATION LEVELS DURING CONSTRUCTION

	PPV (in/sec)				
Equipment	@ 25	@ 100′	@ 300′		
Bulldozer (Large)	0.089	0.019	0.006		
Bulldozer (Small)	0.003	0.0006	0.0002		
Loaded Truck	0.076	0.017	0.005		
Jackhammer	0.035	0.008	0.002		
Vibratory Roller	0.210	0.046	0.013		
Caisson Drilling	0.089	0.019	0.006		
Source: Caltrans	·				

Project demolition and construction activities would not be expected to produce continuous vibration levels exceeding the City's criterion of 0.20 in/sec PPV at nearby sensitive receptor locations. After full project build out, it is not expected that ongoing operational activities will result in any vibration impacts at nearby sensitive uses. Activities involved in trash bin collection could result in minor on-site vibrations as the bin is placed back onto the ground. Such vibrations would not be expected to be felt at the closest off-site sensitive uses. Additional mitigation is not required.

Potential Impact: Vibration impacts could occur if the project were to include pile driving or vibratory roller activities.

Mitigation Measure: If used during project construction, vibratory rollers must not be used within 30 feet of any existing structures.

Mitigation Measure: According to the project applicant, pile driving activities would not occur as part of project construction. The City of San Jose states that the use of an impact driver should not be used within 125 feet of an existing structure. If construction plans regarding pile driving activities were to change, a detailed soil and vibration analysis may be required for City approval.

e. Noise Impacts from Nearby Airports or Airstrips (No Impact)

Norman Y. Mineta San Jose International Airport (SJC) is located approximately two (2) miles north of the project site. WJVA reviewed the airport noise contours provided in the San Jose International Airport Comprehensive Land Use Plan⁴ (dated 11/16/16). The project site is not located within the 65 dB CNEL noise level contour, and therefore does not result in a noise impact associated with airport activities. The SJC Airport noise contours and the location of the project site are provided as Figure 5.

f. Noise Impacts to On-Site Proposed Noise-Sensitive Uses (Less Than Significant)

The General Plan establishes an exterior noise level compatibility standard of 70 dB L_{dn} for office land uses. The exterior noise level standard applies to usable outdoor activity areas, excluding balconies and residential stoops and porches facing existing roadways.

Exterior Noise

The project would include two (2) rooftop terrace use seating areas. The rooftop area would be acoustically shielded from most exterior traffic noise from the building itself. Based upon the noise levels measured at noise monitoring site LT-1 (approximately 56 dB L_{dn}) and acoustical shielding provided by the building, exterior noise levels at the common use rooftop seating areas would be expected to be approximately 45-50 dB L_{dn} .

5. <u>IMPACT SUMMARY</u>

Operational exterior noise levels associated with the proposed project would be limited to human voices within outdoor terrace areas as well as noise associated with mechanical/HVAC systems. All mechanical/HVAC system equipment would be roof mounted or contained within the building itself. HVAC noise levels would be expected to be below 50 dB at the adjacent residential land uses. The majority of vehicle movements would be limited to below grade parking area, and vehicle noise would not be expected to exceed any City of Sana Jose noise level standards. Operational noise associated with the project itself would not be expected to exceed 60 dB L_{dn} (General Plan) or 55 dB L_{max} (Municipal Code) at any adjacent or nearby residential land uses.

This impact summary addresses only the noise impacts determined to be "potentially significant" and summarizes the mitigation measures that would be required to reduce noise levels to a "less than significant" level. Project-related noise levels resulting from the proposed project are not expected to exceed any applicable City of San Jose noise level standards if proper mitigation measures are incorporated into project construction operations. Potential impacts and correlating mitigation measures are described in detail above, and summarized below.

Potential Impact: If the overall duration of construction activities were to occur over a period greater than twelve months, a noise impact would occur, as determined by the City of San Jose Municipal Code.

Mitigation Measure: The anticipated duration of project construction (including demolition) is less than twelve months. However, if project construction were to occur for a duration greater than twelve months, the project team must provide a construction noise logistics plan that specifies hours of construction, noise and vibration minimization measures, posting or notification of construction schedules, and designation of a noise disturbance coordinator who would respond to neighborhood complaints will be required to be in place prior to the start of construction and implemented during construction to reduce noise impacts on neighboring residents and other uses.

Potential Impact: Vibration impacts could occur if the project were to include pile driving or vibratory roller activities.

Mitigation Measure: If used during project construction, vibratory rollers must not be used within 30 feet of any existing structures.

Mitigation Measure: According to the project applicant, pile driving activities would not occur as part of project construction. The City of San Jose states that the use of an impact driver should not be used within 125 feet of an existing structure. If construction plans regarding pile driving activities were to change, a detailed soil and vibration analysis may be required for City approval.

6. SOURCES CONSULTED

- 1. Envision San Jose 2040 General Plan, November 2011.
- 2. San Jose Municipal Code, 2000.
- 3. California Department of Transportation, *Transportation and Construction Vibration Guidance Manual*, September 2013.
- 4. Federal Highway Administration, *Traffic Noise Model, Version 2.5,* April 14, 2004
- 5. San Jose International Airport Comprehensive Land Use Plan[,] November 16, 2016.

FIGURE 1: PROJECT FLOOR PLAN

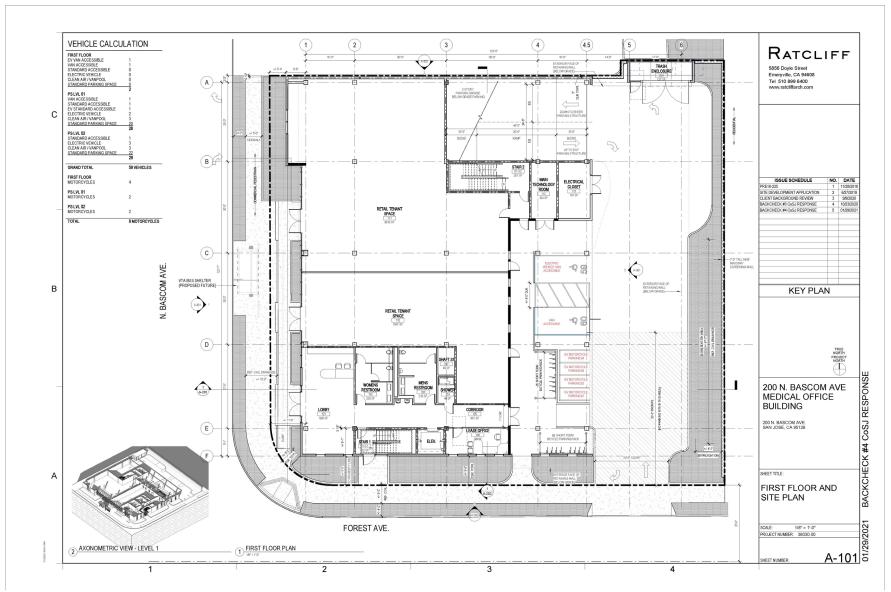


FIGURE 2: PROJECT VICINITY AND AMBIENT NOISE MONITORING SITES

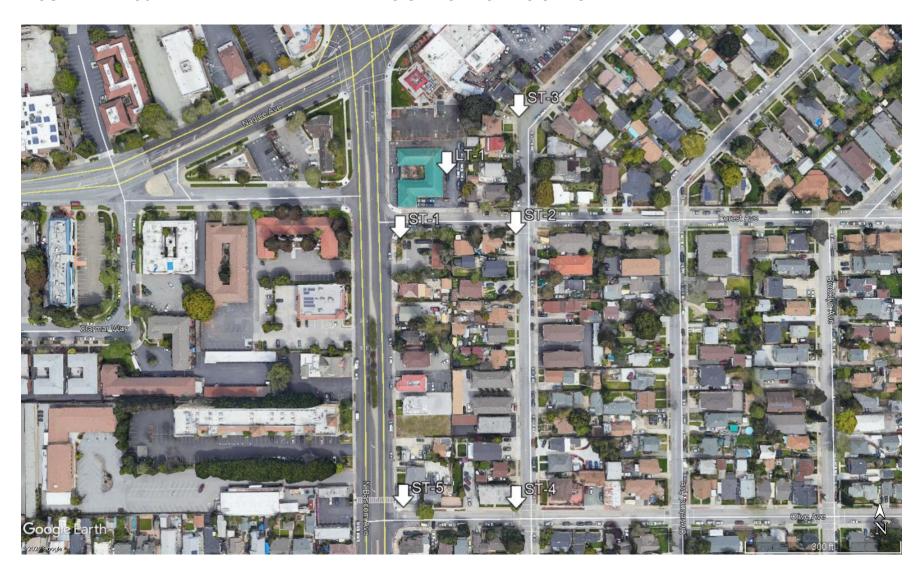


FIGURE 3: HOURLY NOISE LEVELS AT LONG-TERM MONITORING SITE LT-1

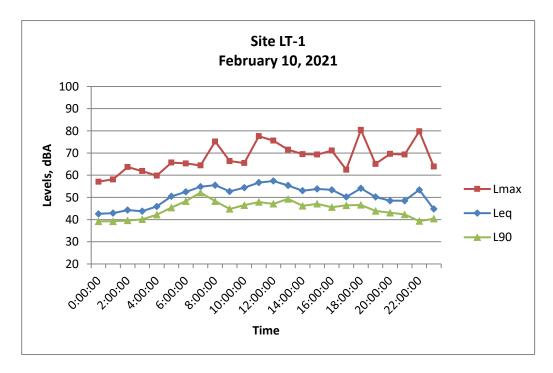




FIGURE 4: LOCATIONS OF MODELED TRAFFIC NOISE RECEPTORS

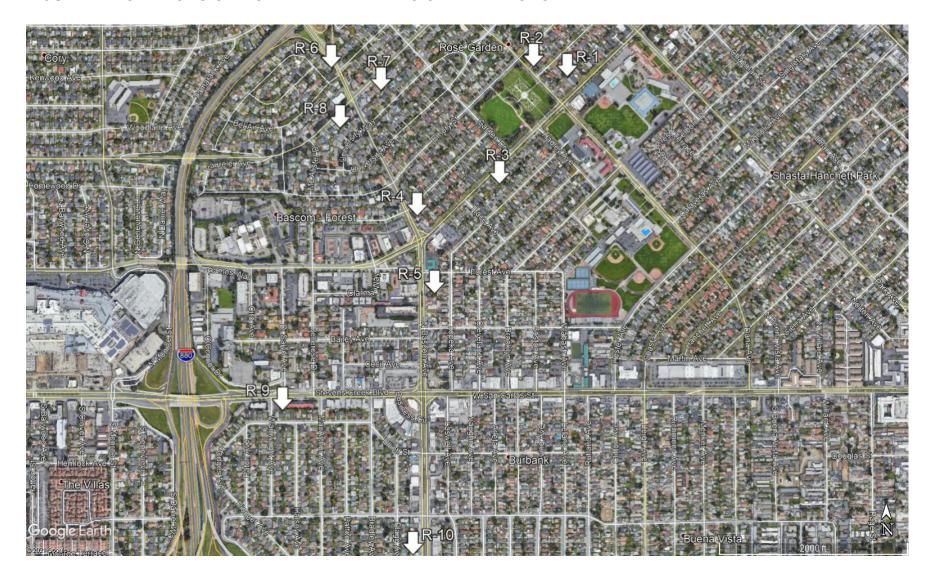
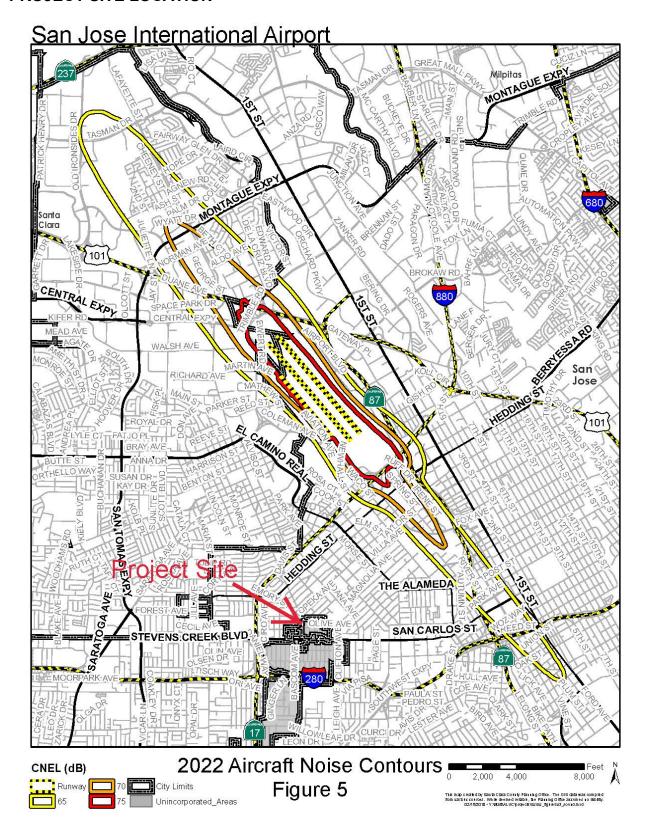


FIGURE 5: SAN JOSE INTERNATIONAL AIRPORT NOISE CONTOURS AND PROJECT SITE LOCATION



APPENDIX A-1

ACOUSTICAL TERMINOLOGY

AMBIENT NOISE LEVEL: The composite of noise from all sources near and far. In this

context, the ambient noise level constitutes the normal or existing

level of environmental noise at a given location.

CNEL: Community Noise Equivalent Level. The average equivalent sound

level during a 24-hour day, obtained after addition of approximately five decibels to sound levels in the evening from 7:00 p.m. to 10:00 p.m. and ten decibels to sound levels in the

night before 7:00 a.m. and after 10:00 p.m.

DECIBEL, dB: A unit for describing the amplitude of sound, equal to 20 times the

logarithm to the base 10 of the ratio of the pressure of the sound measured to the reference pressure, which is 20 micropascals (20

micronewtons per square meter).

DNL/L_{dn}: Day/Night Average Sound Level. The average equivalent sound

level during a 24-hour day, obtained after addition of ten decibels to sound levels in the night after 10:00 p.m. and before 7:00 a.m.

L_{eq}: Equivalent Sound Level. The sound level containing the same total

energy as a time varying signal over a given sample period. Leg is

typically computed over 1, 8 and 24-hour sample periods.

NOTE: The CNEL and DNL represent daily levels of noise exposure

averaged on an annual basis, while Leg represents the average noise

exposure for a shorter time period, typically one hour.

Lmax: The maximum noise level recorded during a noise event.

L_n: The sound level exceeded "n" percent of the time during a sample

interval (L₉₀, L₅₀, L₁₀, etc.). For example, L₁₀ equals the level

exceeded 10 percent of the time.

A-2

ACOUSTICAL TERMINOLOGY

NOISE EXPOSURE CONTOURS:

Lines drawn about a noise source indicating constant levels of noise exposure. CNEL and DNL contours are frequently utilized to describe community exposure to noise.

NOISE LEVEL REDUCTION (NLR):

The noise reduction between indoor and outdoor environments or between two rooms that is the numerical difference, in decibels, of the average sound pressure levels in those areas or rooms. A measurement of Anoise level reduction" combines the effect of the transmission loss performance of the structure plus the effect of acoustic absorption present in the receiving room.

SEL or SENEL:

Sound Exposure Level or Single Event Noise Exposure Level. The level of noise accumulated during a single noise event, such as an aircraft overflight, with reference to a duration of one second. More specifically, it is the time-integrated A-weighted squared sound pressure for a stated time interval or event, based on a reference pressure of 20 micropascals and a reference duration of one second.

SOUND LEVEL:

The sound pressure level in decibels as measured on a sound level meter using the A-weighting filter network. The A-weighting filter de-emphasizes the very low and very high frequency components of the sound in a manner similar to the response of the human ear and gives good correlation with subjective reactions to noise.

SOUND TRANSMISSION CLASS (STC):

The single-number rating of sound transmission loss for a construction element (window, door, etc.) over a frequency range where speech intelligibility largely occurs.

APPENDIX B EXAMPLES OF SOUND LEVELS

SUBJECTIVE NOISE SOURCE SOUND LEVEL **DESCRIPTION** 120 dB AMPLIFIED ROCK 'N ROLL > **DEAFENING** JET TAKEOFF @ 200 FT ▶ 100 dB **VERY LOUD** BUSY URBAN STREET > 80 dB **LOUD** FREEWAY TRAFFIC @ 50 FT > CONVERSATION @ 6 FT ▶ 60 dB **MODERATE** TYPICAL OFFICE INTERIOR > 40 dB SOFT RADIO MUSIC > **FAINT** RESIDENTIAL INTERIOR > WHISPER @ 6 FT ▶ 20 dB **VERY FAINT** HUMAN BREATHING > 0 dB

APPENDIX C TRAFFIC NOISE MODELING CALCULATIONS

ht	%Med	%Heavy	Speed	Distance	Offset
10	2	1	35	80	
10	2	1	35	170	
10	2	1	35	75	
10	2 2 2 2 2 2	1	35	130	
10	2	1	35	140	
10	2	1	35	60	
10	2	1	35	120	
10	2 2	1	35	140	
10		1	35	130	
10	2	1	35	160	

Roadway Name	Segment Description	ADT	%Day	%Evening
Dana Ave	n/o Naglee Ave R-2	2170	90	
Naglee Ave	e/o Dana Ave R-1	13330	90	
Bascom Ave	n/o Naglee Ave R-4	19710	90	
Bascom Ave	s/o Naglee Ave R-5	19590	90	
Naglee Ave	e/o Bascom Ave R-3	14370	90	
Bascom Ave	n/o Hedding St R-6	21960	90	
Hedding St	w/o Bascom Ave R-8	12340	90	
Hedding St	e/o Bascom Ave R-7	12520	90	
Bascom Ave	s/o San Carlos St R-10	25120	90	
Stevens Creek Blvd	w/o Bascom Ave R-9	15230	90	
	1	1		

WJV Acoustics, Inc FHWA-RD-77-108 Calculation Sheets March 4, 2021

Project #: 21-08

Description: Ldn/Cnel: Existing plus project Ldn Soft Site Type:

Contour Levels (dB) 60 65

70 75

Segmen	t
	1
	2
	3
	4
	5
	6
	7
	8
	^

10

Roadway Name	Segment Description	ADT	%Day	%Evening
Dana Ave	n/o Naglee Ave R-2	2190	90	
Naglee Ave	e/o Dana Ave R-1	13380	90	
Bascom Ave	n/o Naglee Ave R-4	20190	90	
Bascom Ave	s/o Naglee Ave R-5	20350	90	
Naglee Ave	e/o Bascom Ave R-3	14370	90	
Bascom Ave	n/o Hedding St R-6	22240	90	
Hedding St	w/o Bascom Ave R-8	12440	90	
Hedding St	e/o Bascom Ave R-7	12620	90	
Bascom Ave	s/o San Carlos St R-10	25170	90	
Stevens Creek Blvd	w/o Bascom Ave R-9	15520	90	

10	ıt	%Med	%Heavy	Speed	Distance	Offset
10 2 1 35 75 10 2 1 35 130 10 2 1 35 140 10 2 1 35 60 10 2 1 35 120 10 2 1 35 140 10 2 1 35 140 10 2 1 35 130	10	2	1		80	
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WJV Acoustics, Inc FHWA-RD-77-108 **Calculation Sheets** March 4, 2021

21-08 Project #: Description: Background no project

Ldn/Cnel: Ldn Site Type: Soft Contour Levels (dB)

65 70 75

Segment 2

> 9 10

Roadway Name	Segment Description	ADT
Dana Ave	n/o Naglee Ave R-2	24
Naglee Ave	e/o Dana Ave R-1	1348
Bascom Ave	n/o Naglee Ave R-4	206
Bascom Ave	s/o Naglee Ave R-5	204
Naglee Ave	e/o Bascom Ave R-3	1532
Bascom Ave	n/o Hedding St R-6	227
Hedding St	w/o Bascom Ave R-8	129
Hedding St	e/o Bascom Ave R-7	128
Bascom Ave	s/o San Carlos St R-10	258
Stevens Creek Blvd	w/o Bascom Ave R-9	184

ght	%Med	%Heavy	Speed	Distance	Offset
10	2	1	35	80	
10	2	1	35 35	170	
10	2	1	35	75	
10	2	1	35	130	
10	2 2 2	1	35	140	
10	2	1	35	60	
10		1	35	120	
10	2	1	35	140	
10	2	1	35	130	
10	2	1	35	160	

Roadway Name	Segment Description	ADT	%Day	%Evening	%Night	%M
Dana Ave	n/o Naglee Ave R-2	2470	90		10	
Naglee Ave	e/o Dana Ave R-1	13480	90		10	
Bascom Ave	n/o Naglee Ave R-4	20620	90		10	
Bascom Ave	s/o Naglee Ave R-5	20490	90		10	
Naglee Ave	e/o Bascom Ave R-3	15320	90		10	
Bascom Ave	n/o Hedding St R-6	22740	90		10	
Hedding St	w/o Bascom Ave R-8	12910	90		10	
Hedding St	e/o Bascom Ave R-7	12880	90		10	
Bascom Ave	s/o San Carlos St R-10	25810	90		10	
Stevens Creek Blvd	w/o Bascom Ave R-9	18410	90		10	
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WJV Acoustics, Inc FHWA-RD-77-108 Calculation Sheets March 4, 2021 Contour Levels (dB) 21-08 Project #: Description: Background plus project Ldn/Cnel: Ldn Site Type: Soft Segment Roadway Name **Segment Description** ADT %Day %Evening %Night %Med %Heavy Speed Distance Offset Dana Ave n/o Naglee Ave R-2 Naglee Ave e/o Dana Ave R-1 Bascom Ave n/o Naglee Ave R-4 s/o Naglee Ave R-5 Bascom Ave Naglee Ave e/o Bascom Ave R-3 n/o Hedding St R-6 Bascom Ave Hedding St w/o Bascom Ave R-8 e/o Bascom Ave R-7 Hedding St Bascom Ave s/o San Carlos St R-10 Stevens Creek Blvd w/o Bascom Ave R-9